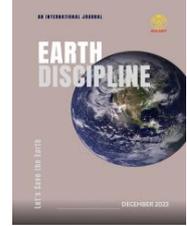


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Review Article

A Thorough Examination of Ignition Engines with Homogenous Charge Compression

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ABSTRACT

An innovative form of combustion technology is employed by homogeneous charge compression ignition (HCCI) engines. In theory, after the mixture reaches the temperature required for autoignition, combustion occurs at several locations without the assistance of a spark plug or injector. In order to successfully operate an HCCI mode engine, it is necessary to overcome the following challenges: managing the mixture's homogeneous charge preparation, cold start, auto-ignition, operating range, regulating knock and emissions of unburned hydrocarbon (UHC) and carbon monoxide (CO). This study analyzes the knocking in the HCCI combustion and discusses the HCCI mode engine's operating concept. Additionally, examine how homogeneous charge affects HCCI combustion characteristics like maximum pressure and heat release rate. Examines, however, the engine's performance and emission characteristics. The specialised literature reports a comparative evaluation of emission and performance for each of these parameters, along with a discussion of the theories pertaining to the successful operation of HCCI engines.

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Introduction

Internal combustion engine were used extensively in the many different contexts all over the world. Technology for homogeneous charge compression ignition engines is one potential choice for a unique combustion modes that could reduce the pollution levels from these engines. By compressing a homogenous mixture of fuel and air until auto-ignition happens close to the conclusion of the compression stroke, the HCCI technology allows for substantially faster combustion than either spark ignition and compression ignition. SI engines' limited efficiency at partial loads is its main drawback. SI engines have a limited compression ratio due to knock, typically falling between 8 and 12, which contributes to their low efficiency. Standard diesel engines operate at lower compression ratios than do SI engines, which is a classic example of CI combustion. Instead of using a spark plug for ignite the air fuel mixture in this type of engine, the piston compression causes it to do so automatically.

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A number of intricate processes occur between the moment the liquid fuel leaves the injector nozzles and when it starts to and vapour diffusion, collisions, involving droplet formation, burn and destruction, evaporation. These mechanisms essentially restrict the rate of combustion. A greater percentage of the fuel will have a longer time scale for diffusion and evaporation etc. than for chemical reactions even though some of the fuel and air will be mixed and burn quickly. Consequently, areas with high fuel concentration and regions with high flame temperature can be distinguished within the mixture. Because there is no oxygen present, a lot of soot forms in the areas with high fuel concentrations. The increased in-cylinder temperature has the potential to oxidize some soot. Conventional diesel engines have an in-cylinder temperature of roughly 2700 K, which results in high NO_x emissions. Any fuel or combination of fuels can be used to alter either SI or CI engines to apply HCCI technology, which promises to increase engine thermal efficiency while maintaining low emissions. HCCI engines typically have a lean air/fuel mixture quality that auto-ignites in several places before burning volumetrically without showing signs of flame propagation. In contrast to spark or injection timing, combustion occurs the homogeneous fuel mixture reaches the chemical activation energy and is entirely controlled by chemical kinetics.

Developing HCCI engines presents new difficulties because of the lean mixture, which is entirely controlled by chemical kinetics. It is challenging to meet emission standards, control knock, achieve cold start and manage the mixture's auto-ignition and heat release rate during high load operation. The benefits of incorporating HCCI technology into IC engines involve the capacity to run on a variety of fuels, excellent efficiency in comparison to SI engines that approaches the efficiency of CI engines, and flexibility to any engine configuration—car, stationary, heavy duty, or small. Conversely, there are a few drawbacks to HCCI engines, including high level of unburned hydrocarbons (UHC) and carbon monoxide (CO) as well as knocking under specific operating circumstances. The efficiency of HCCI engines has been nearly restored to that of CI engines despite the fact that pollution rules are getting stricter and that the NO_x and soot emissions levels have been drastically decreased. However, due to its abrupt onset, knocking continues to be the main problem. When an engine reaches top dead center (TDC) too soon, it can cause knocking, which lowers engine reliability because of excessive vibration.

The fuel type has a significant impact on an HCCI engine's performance, which also has an impact on emissions. As one of the variables influencing engine technology nowadays is pollution levels, HCCI development has advanced to a new level. Reports on the latest advancements in HCCI engines are necessary because of the significance of this technology, which has the potential to replace traditional SI and CI engines. This study examines the fundamental functioning of the HCCI engine in addition to the combustion variables, such as heat release rate and maximum pressure throughout the combustion process. Nonetheless, an analysis of the knocking in HCCI combustion and a discussion of the knocking controlling parameter followed. This document also briefly discusses the HCCI engine's performance and emission characteristics.

REVIEW OF LITERATURE

The HCCI engine has been the subject of extensive research. Listed below are a few of them.

Homogeneous mixture preparation was accomplished by Rakesh Kr Maurya using the port fuel injection technique. The two-cylinder engine was changed to operate in the homogenous charge compression ignition mode, with one cylinder operating as a standard compression ignition diesel engine and the other as a twin-cylinder engine. At constant speed of 1570 rpm, experiments were conducted to establish steady HCCI combustion by varying the equivalency ratio and intake charge temperature. It was discovered that within the air-fuel ratio ranges from 2.1 to 5.7 stable homogenous charge combustion was accomplished. The greatest indicated thermal efficiency of 45.42 % was obtained by ethanol, which had the maximum IMEP of 4.4 bar at 2.7 air fuel ratio and 112^oC intake air temperature. We also discussed the properties of combustion, efficiency of combustion, and emissions. A study on the experimental blending of ethanol in biodiesel was carried out by Haoyue Zhu et al. [2]. Ethanol addition increased wave development and interaction at the liquid-gas interface while decreasing viscosity and surface tension. To achieve a more uniform composition, add ethanol and enhance spray atomization. One-cylinder engine testing were carried out using a modified multi-CIDI engine. The reduction of soot and biodiesel–ethanol, biodiesel and NO_x for diesel was the focus of their efforts.

Premixed low temperature combustion (LTC) mode in a moderate exhaust gas recirculation (EGR) was studied. The study concentrated on blended ethanol and found that it improved the rate of fuel and air mixing, extended the ignition delay, and raised fuel oxygen from 10.2% to 15.1% due to a decrease in soot.

An experimental investigation was carried out by Vittorio Manente et al. [3] to perform a sweep at high load during the beginning of the pilot and pilot-main interaction ratio injection. The most practical stratification level that maximized efficiency and decreased emissions was determined by conducting a start of injection SOI sweep. Based on a single-cylinder DI engine that had been modified, the experiment used compressed air on an external airline to boost the engine. An injection mechanism made by Bosch was used to inject fuel. Ethanol (97.9 % by volume, heating value of 28.7 MJ/kg) was the fuel used. At various operational parameters, they carry out both high and low load analyses. As a result of varying the EGR rate between 42 to 49% and the air fuel ratio between 1.25 and 1.35, low levels of CO, soot, HC and NO_x were shown to be achievable. At -61° TDC, pilot injections were made, and a 50-50 pilot main ratio was discovered. The amount of soot produced could be decreased by using some oxygenate.

The impact of ethanol's water fraction on the working limitations of HCCI engines, as well as the intake exhaust emissions, heat release rate and temperature was examined by J. Hunter Mack et al., [4]. The VW 1.87 L 4-cylinder engine was used for the testing. The MSD software was used to control the port injection of liquid fuels using an MSD injector. With changing fractions of 40%, 60%, 80%, 90% and 100% of ethanol in water mixtures, ethanol fuel flow rates were maintained constant during all experiments. It was determined that stable HCCI functioning was achieved for fuels comprising up to 40% water. The results showed that a high percentage of water to ethanol may be run in an engine by raising the intake heating value.

The use of wet ethanol as a fuel for homogenous charge compression ignition engines was the main subject of Samveg Saxena et al.'s study [5]. by raising the temperature and supplying the high input energy needed to ignite wet ethanol through the use of exhaust heat recovery. Since the primary expense of extracting ethanol is distillation, this cost increased while extracting the fuel's low water content. At 1800 rpm, a 1.9L Volkswagen TDI engine with four cylinders was used for the testing. A few modifications were made to the piston of this experimental engine to lower heat loss. With a precise pressure regulator, intake air was supplied by an external high pressure compressor equipped with a 7.2 m³ surge tank. The results showed that high intake pressure and high equivalency ratio were the best conditions for employing wet ethanol in an HCCI engine with exhaust heat recovery. Use of exhaust heat recovery with 1.4–2 bar of intake pressure and a 0.25–0.55 fuel-to-air ratio allows for the utilization of 20% water in fuel. A higher intake temperature will result in earlier combustion timing, which will further advance the combustion timing. A lower exhaust temperature will also produce a decrease in intake temperature, which will result in later combustion timing.

The mixture was created outside of the combustion chamber by D. Ganesh et al. [6]. Equal parts air and vaporized diesel fuel were introduced to the combustion chamber during the intake stroke. In addition to adding a vaporizer, an ECU to control the port fuel injection system, exhaust gas recirculation, a DAS, a fuel metering system, and a crank angle encoder, they adapted a single-cylinder diesel engine to function in the HCCI mode. Initially, the engine was started in the traditional manner, and fuel was pumped externally so that mechanical. They experimented with diesel vapour induction without EGR and with 30%, 20% and 10% EGR to control ignition. Findings demonstrated the significance of EGR's involvement in regulating the combustion phase. Governor turns off diesel supplies. Findings demonstrated the significance of EGR's involvement in regulating the combustion phase. The expulsion gas recirculation system's combustion phasing is quite sensitive because EGR was used to reduce the cylinder pressure and temperature. The rate of pressure rise in the combustion chamber and combustion control are significantly influenced by EGR. With the stated rise in EGR%, brake thermal efficiency dropped. Although the HCCI lowered NO_x emissions by 91–97 %, it often resulted in approximately 30% higher emissions of HC and CO when compared to a traditional diesel engine.

According to research by Akhilendra Pratap Singh et al. [7], because diesel has less volatility, homogenous mixing of charges is the most challenging aspect of combustion in HCCI powered by diesel. To create a uniform fuel-air combination, they so employed a machine known as a "diesel vaporizer. With the possible exception of an external band heater controlled by a PID temperature controller and the vaporizer was essentially a copper

chamber. While varying the EGR %, experiments were conducted at three distinct relative air-fuel ratios ($k = 4.95, 3.70, \text{ and } 2.56$). They employed a 2-cylinder, 4-stroke DI diesel engine running at a steady pace for the experiment. The other cylinder continued to operate in normal mode, with only one cylinder converted to an HCCI combustion mode. They spoke about the two stages of heat release, the efficient HCCI condition, the start of combustion, and the EGR conditions (0, 10%, and 20%).

Bahram Bahri et al. [8] study concentrated on how misfire affected the combustion phasing matrix, IMEP, trace heat release, and exhaust emissions. It was under discussion if features of the homogeneous charge compression ignition engine powered by ethanol were essential to misfire detection. They detected misfire using an ANN model. Demonstrate by experimentation the model's 100% correctness. They have also experimented with a 4-stroke, single-cylinder CIDI engine that has been converted to HCCI mode. An intake manifold with an air pre warmer (3 KW heater) was installed to enable uniform charges in the cylinder of a fuel premixing system. The timing of the ignition, the formation of misfires and burn length were ascertained. They said that when the HRR of a cycle dropped by 10% or more, it was considered a partial misfire, and when it dropped by less than 50%, it was considered a misfire cycle. This experiment identified three different types of misfires: the first was caused by a lack of fuel; the second by a lean mixture of air and fuel and the third by an inadequate temperature. According to the findings, the homogenous charge combustion matrix's dissimilarity and equivalency ratio had an effect on the ethanol HCCI. The maximum HRR and IMEP were shown to be closely connected. The HCCI misfire detection parameters, cyclic SOC, CASO, and CAMHRR, are ineffective.

In their review, Suyin Gan et al. [9] examined how HCCI combustion functions in CIDI engines with varying injection methods in relation to crank angle and time. For instance, early injection, repeated injections, late injection tactics, physical variations such as injector properties, cylinder and piston shape, compression ratio, and swirl ratio. Apart from talking about how design and operating factors like EGR and intake air temperature affect the emissions of HCCI diesel, especially the soot and NO_x that are released during combustion, they also stated that the most important characteristic of HCCI is uniformity of charge.

The quality of fuel was examined by L. Starcket al. [10] in order to improve engine performance. Explain the fuel matrix and the HCCI index. The foundation of these indexes was a comparison between the tested gasoline and the reference fuel, which in this case was EN590 (cetane no. 51.5). According to the findings, the operational limit of the HCCI may be improved by more than 30% using a low cetane number and high volatility fuel with an appropriate chemical composition, all without compromising performance in the conventional diesel combustion mode. They claim that reactive chemicals with low cetane numbers are the best fuel for HCCI performances.

A study by Mingfa Yao et al. [11] was built upon the foundational principles of HCCI engine modeling. Chemical kinetics was explained with a brief discussion of five different kinds of numerical simulation models. Chemical kinetics is the only mechanism that can regulate the HCCI's operating range and combustion initiation. Additionally, they assessed control strategies of diesel-fueled HCCI and how they affected combustion processes. The obstacles and difficulties of HCCI combustion were also discussed, involving fuel modification, cold starting, homogenous mixture preparation, operation range, combustion phasing control, and their implications on chemical kinetics.

To conduct this experiment, Abdul Khaliq et al. [12] modified a basic truck engine. For an ignition engine that runs on ethanol with a water component, they combined the application of the laws of thermodynamics. The impacts of ambient temperature, turbocharger compressor ratio and compressor adiabatic efficiency on first law efficiency, energy destruction and second law efficiency in each component were investigated numerically.

According to P. Alakshminarayanan et al. [13], the relationship between the mixing rate and the turbulent energy generated at the nozzle's end was used to particularly show the rate of combustion. It depends on the injection velocity as well as how energy dissipates next to the cylinder wall and in the open. The complete absence of tuning constants allowed the model to truly stand out from other zero-dimensional or pseudo-multi-dimensional models.

Onishi S. et al. [14] conducted the initial research on HCCI. The experiments were conducted with a 2-stroke gasoline engine. It was reported that the recently developed combustion system known as "Active Thermo-Atmosphere Combustion" (ATAC) produces immediate combustion that is distinct from the combustion processes of traditional SI and CI engines. He explained how an equivalence ratio temperature map has been conceptualized to represent the locations of formation for both NO_x and soot.

The multi-dimensional mathematical method that Annarita Viggiano et al. [15] proposed, together with a kinetic reaction mechanism for ethanol oxidation, CO emissions and NO_x generation were important contributions to their work. Using code and numerical techniques, this model assessed the turbulent and kinetic timescales. They arrived at an optimal solution by solving the system of governing equations. The variability in the cylinder close to the surface was the only factor connecting these contaminants. Understanding the characteristics of HCCI in homogeneities in the combustion chamber, temperature chemical properties and their impact on emissions along performance parameters and ignition delay prediction are all made possible by this study. The researchers investigated temperature in homogeneities, emissions, and wall heat transmission.

CONCLUSION

This review examined the features of combustion, namely the maximum pressure increase and heat release rate in HCCI engine combustion as well as the functioning of the homogeneous charge compression ignition engine. Analyze the HCCI combustion knocking issue in the interim and talk about controlling techniques. Additionally, it examines the HCCI mode engine's emissions and performance characteristics before drawing the following conclusion.

The new combustion technologies have been used in homogeneous charge compression ignition engines. While both SI and HCCI engines use premixed charges to operate, the HCCI mode engine functions similarly to both SI and CI engines. Additionally, it functions similarly to a CI engine in that gasoline ignites automatically to start combustion.

With a knocking sound that coincides with an extreme rise in pressure and rate of heat release, the HCCI engine starts the combustion process. Even though the entire combustion chamber air fuel combination is idealized as igniting uniformly and automatically in an instant, in reality, ignition occurs at different locations inside the mixture one after the other over the course of a short time. The literature revealed that the inlet air temperature, properties of the fuel, exhaust gas recirculation (EGR) and the variable compression ratio (VCR) all had an impact on knocking.

Brake thermal efficiency could be increased by HCCI mode engines since they require less fuel. They run on clean air fuel charge under all operating situations. The HCCI engine produces minimal emissions of NO_x and particles. Nevertheless, it emits more carbon monoxide and unburned hydrocarbons.

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